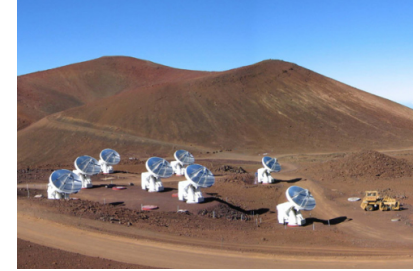




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SMA Wideband Upgrade: Status

Cambridge Staff Members:

*Jack Barrett, Paul Grimes, Robert Kimberk, Steve Leiker, Scott Paine,
Cosmo Papa, Pat Riddle, John Test, Edward Tong*

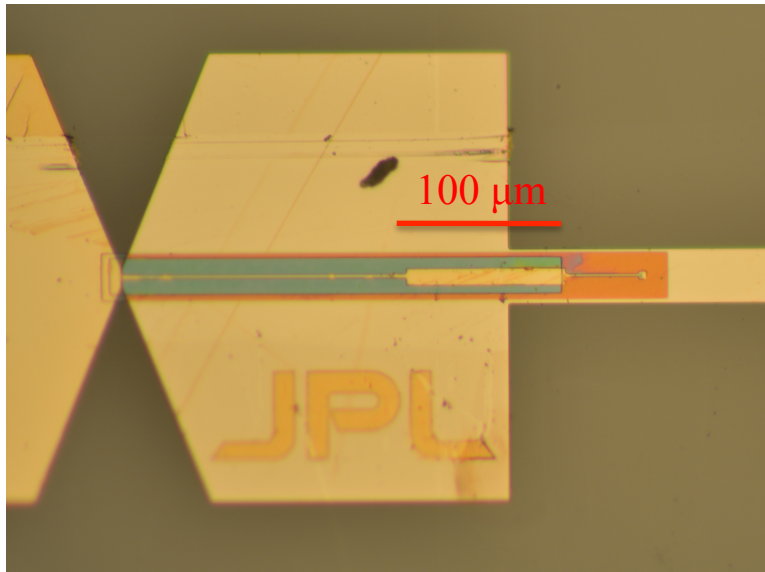
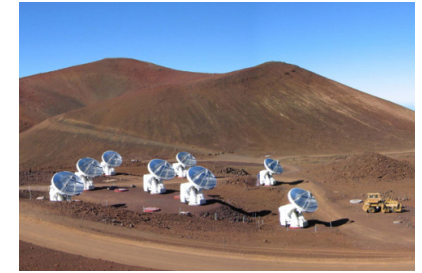
Hilo Staff Members: ALL

ASIAA Staff: *Johnson Han, Ming-Jye Wang, ...*



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SMA 200 GHz Mixer Chip fabricated by JPL in 1990s. Work horse of SMA during its first decade of operation.

IF Bandwidth of SMA:
Initially 4-6 GHz (for 2 receivers)

In late 2000s, we introduced the Bandwidth Doubling module which allows 4 – 8 GHz for single receiver operation.

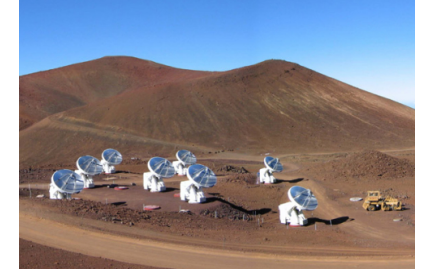
IF Bandwidth was limited by capacity of correlator and output capacitance of SIS mixer.

In 2010, at last Advisory Meeting, we propose to launch a wideband upgrade to provide more IF Bandwidth.

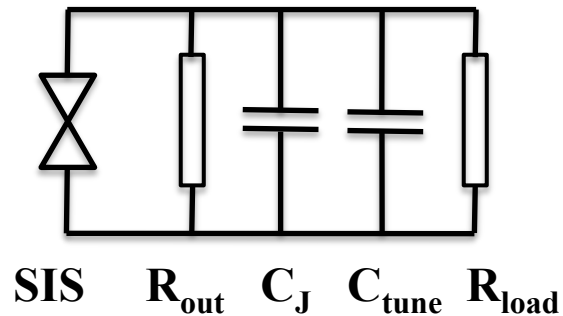


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IF Bandwidth of SIS Mixer



$$IFBW = \frac{1}{2\pi(R_{out} // R_{load})(C_J + C_{tune})}$$

$$\approx \frac{1}{2\pi * 50 * (C_J + C_{tune})} \quad R_{load} = 50 \quad \text{and} \quad R_{out} \gg R_{load}$$

For Original SMA mixer design, $(C_J + C_{tune}) \sim 0.35$ pF,
IFBW ~ 9 GHz

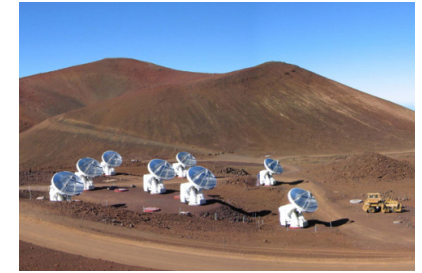
To increase IFBW:

- Reduce Junction Capacitance – **use series junction array.**
- Reduce Tuning Capacitance – **use newer type of tuning circuit.**

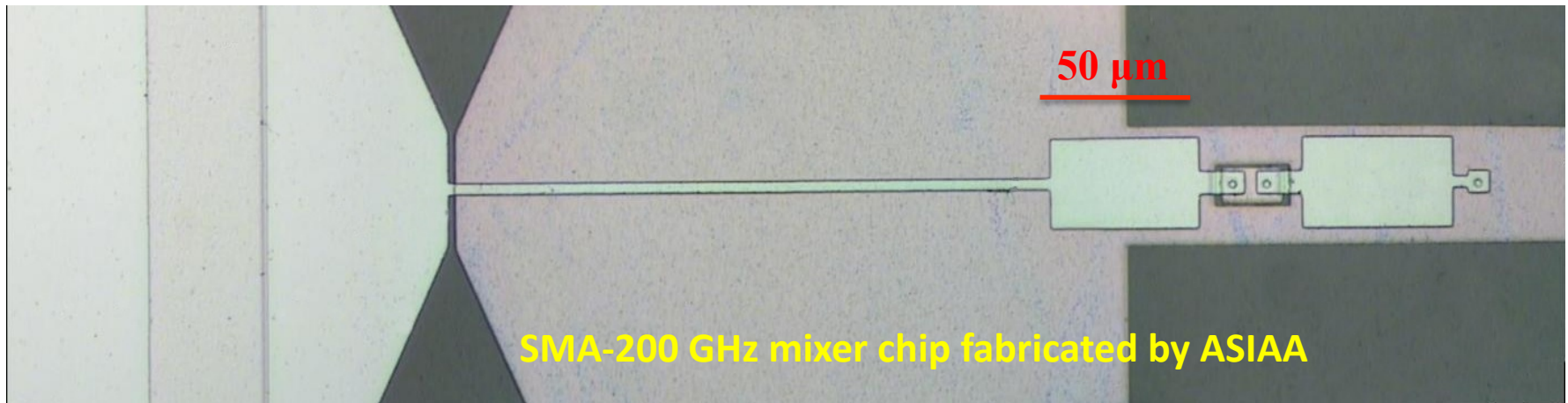


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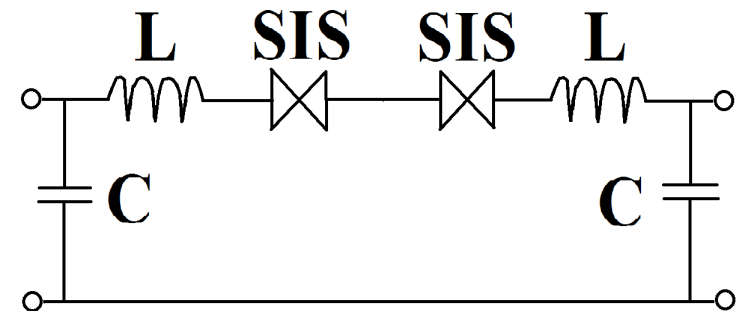
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SMA-200 GHz Wideband Mixer Chip. Version 1



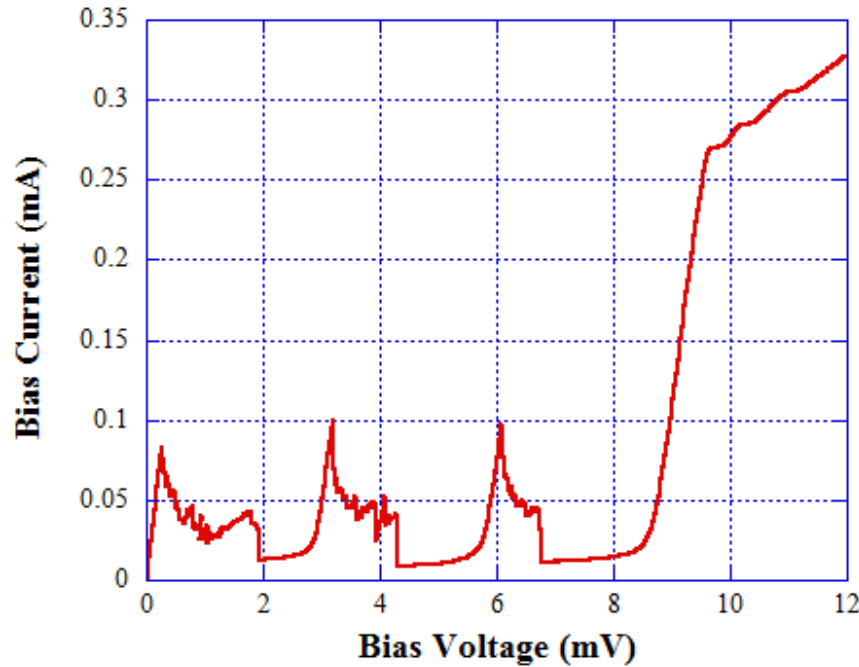
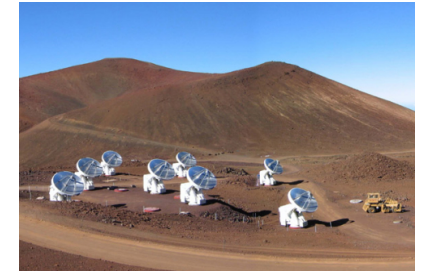
- Transformer-coupled 3-junction design
- Synthesizes a transmission line section
- Current Density: 7 kA/cm²
- Device Size: 1.6 μm diameter
- Resembles end-loaded stub





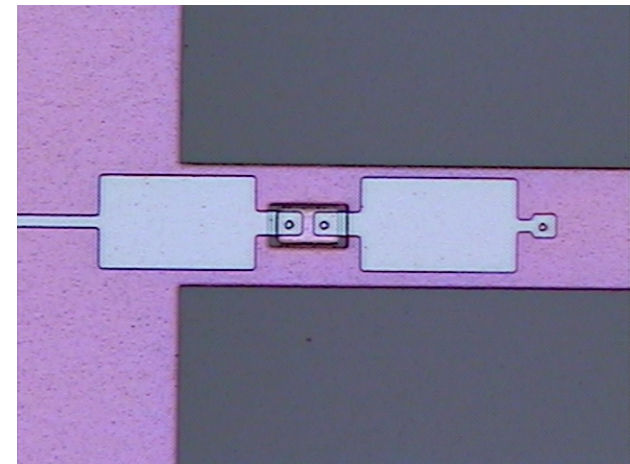
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- $R_N \sim 11 \times 3 \Omega = 33 \Omega$
- $Q > 17$
- $V_{\text{gap}} \sim 2.88 \times 3 \text{ mV} = 8.65 \text{ mV}$
- $C_{\text{out}} \sim 0.25 \text{ pF}$
- projected IF BW $\sim 13 \text{ GHz}$

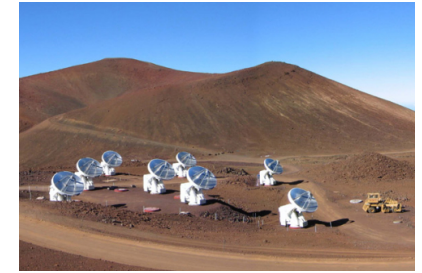
Typical I-V curve of 3-Junction SIS array
produced by ASIAA (2011)
Actual $J_c \sim 8 \text{ kA/cm}^2$



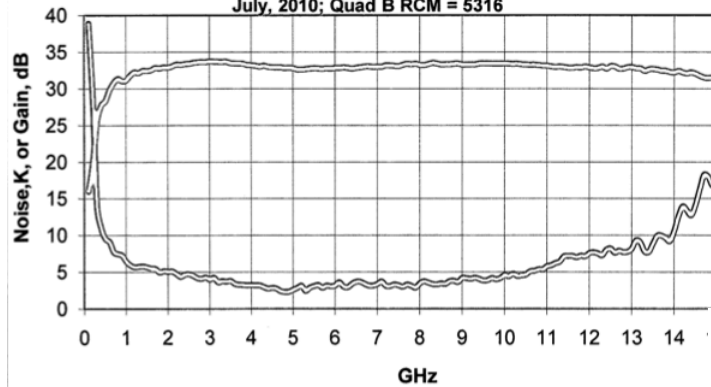


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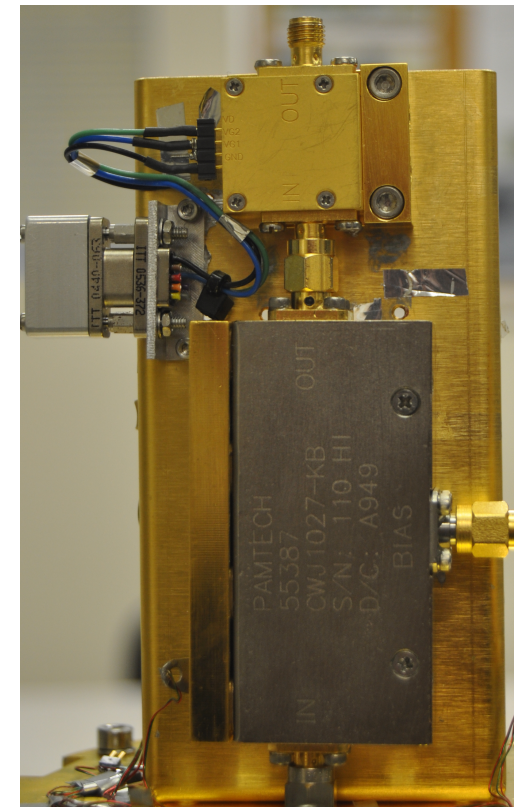
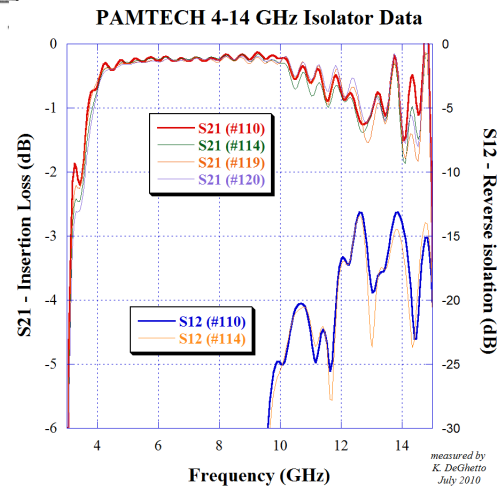
Cryo1-12 SN400D Noise and Gain at 17K
 Vd=1.2V 19.3mA; Vg1= -0.2V Vg2= -0.2V
 July, 2010; Quad B RCM = 5316



Selected units of
 CRYO1-12 features noise
 temp < 5 K up to 11 GHz
 and < 10 K up to 14 GHz.

**PAMTECH/Quinstar 4 – 14 GHz
 isolator is an advanced version of
 the 4 – 12 GHz isolator in use in
 ALMA**

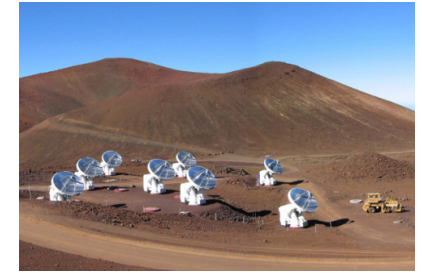
- insertion loss < 0.7 dB
- reverse isolation > 15 dB





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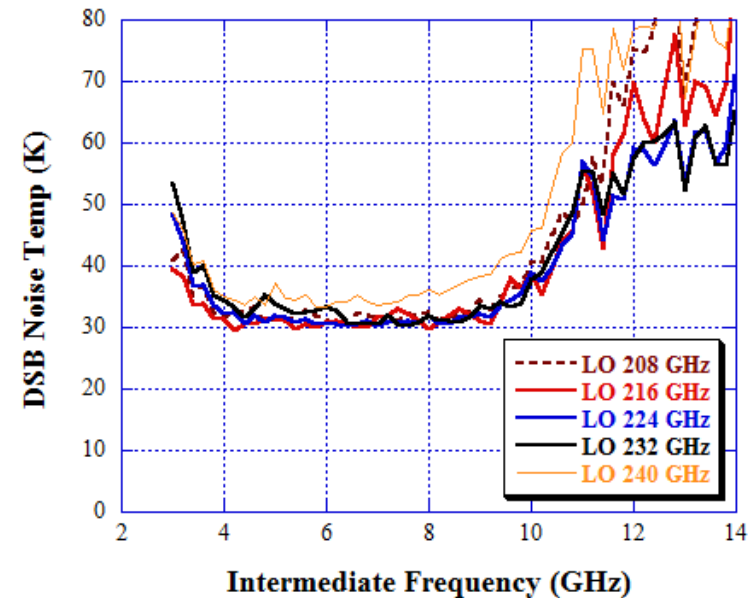
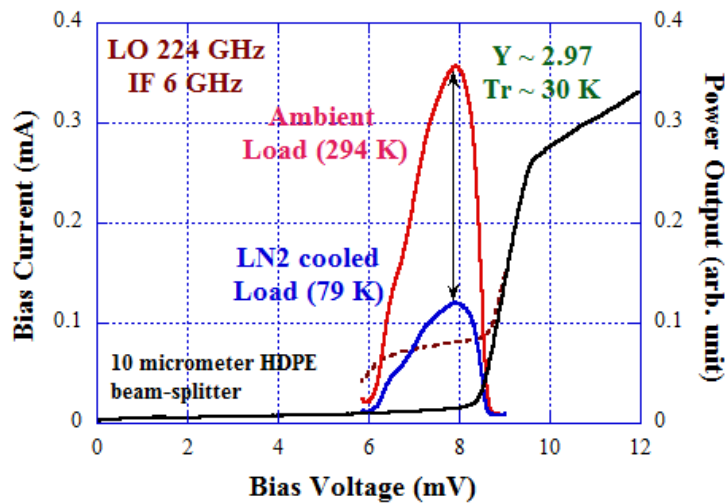
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Laboratory Performance:

- Easy to couple magnetic field (generally operates at 2nd null)
- Rout : 150 – 200 Ω
- Best Y-factor ~ 3 , i.e. $T_{DSB} \sim 30$ K or $h\nu/k \sim 3$

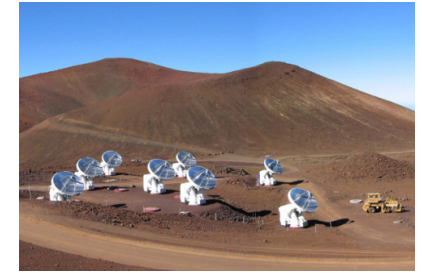
- Smooth P-V except for the lowest LO frequency (too inductive)
- Sensitivity rolls off significantly for $IF > \sim 11$ GHz



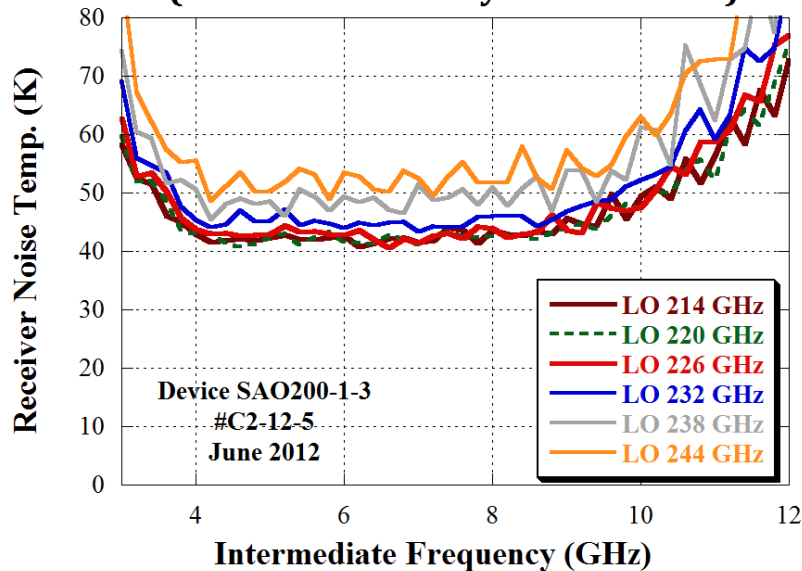


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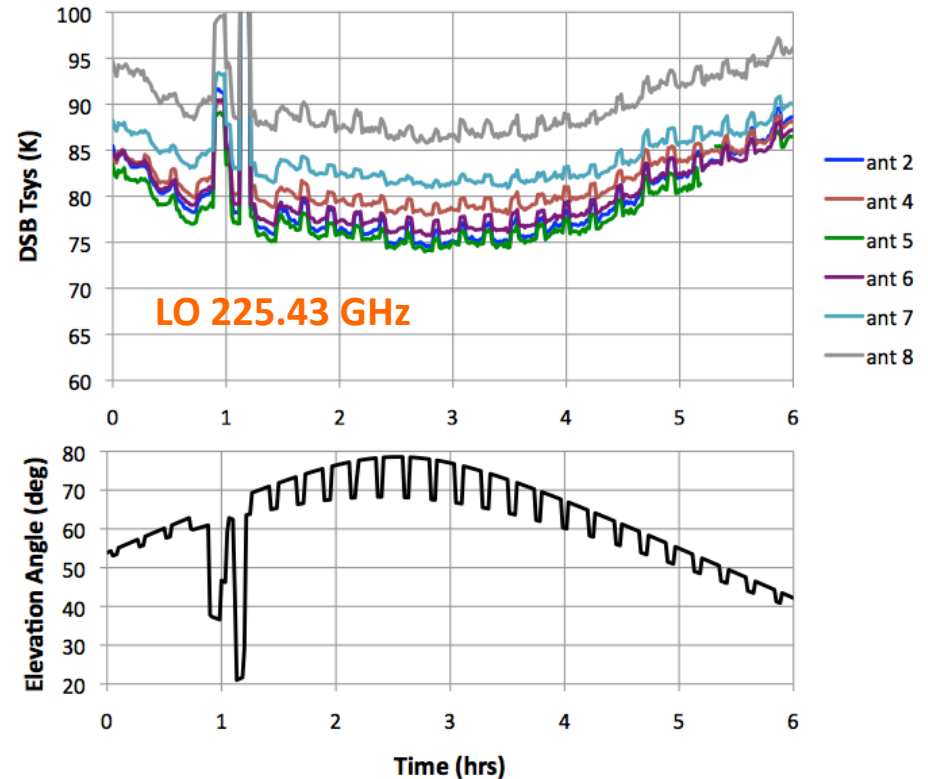


Lab Testing of Receiver Insert 200-C with full SMA Optics (Installed currently in Antenna 6)



All SMA-200 Receivers have been upgraded in 2012 and are being used for routine observation.

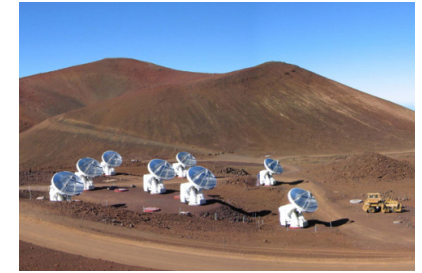
On sky performance of receivers on Jan 10, 2014. Opacity @ 225 GHz ~ 0.05 (good weather) Tsys Value for 4 – 6 GHz Band



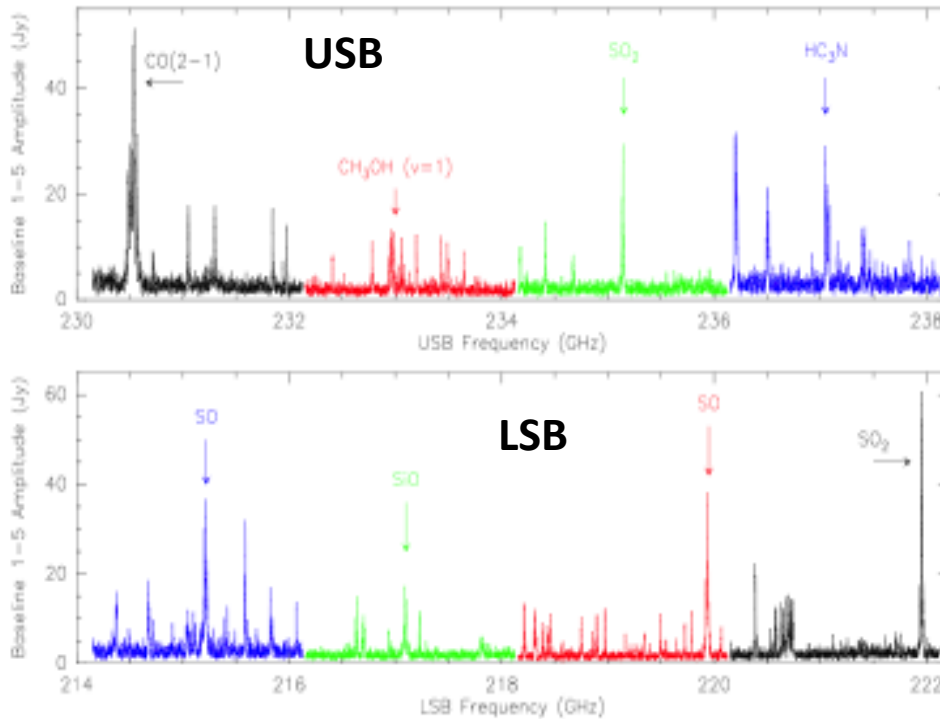


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Test Observation Towards Orion BN/KL LO 226.1 GHz



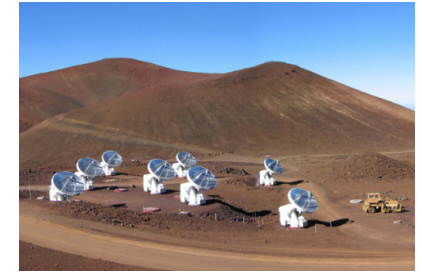
In the absence of the wideband correlator, the upper IF (> 6 GHz) can be read by the existing correlator using an additional downconverter in the BDA module in each antenna.

Any 2 GHz wide IF spectrum falling between 6 and 14 GHz can be mapped to correlator input.

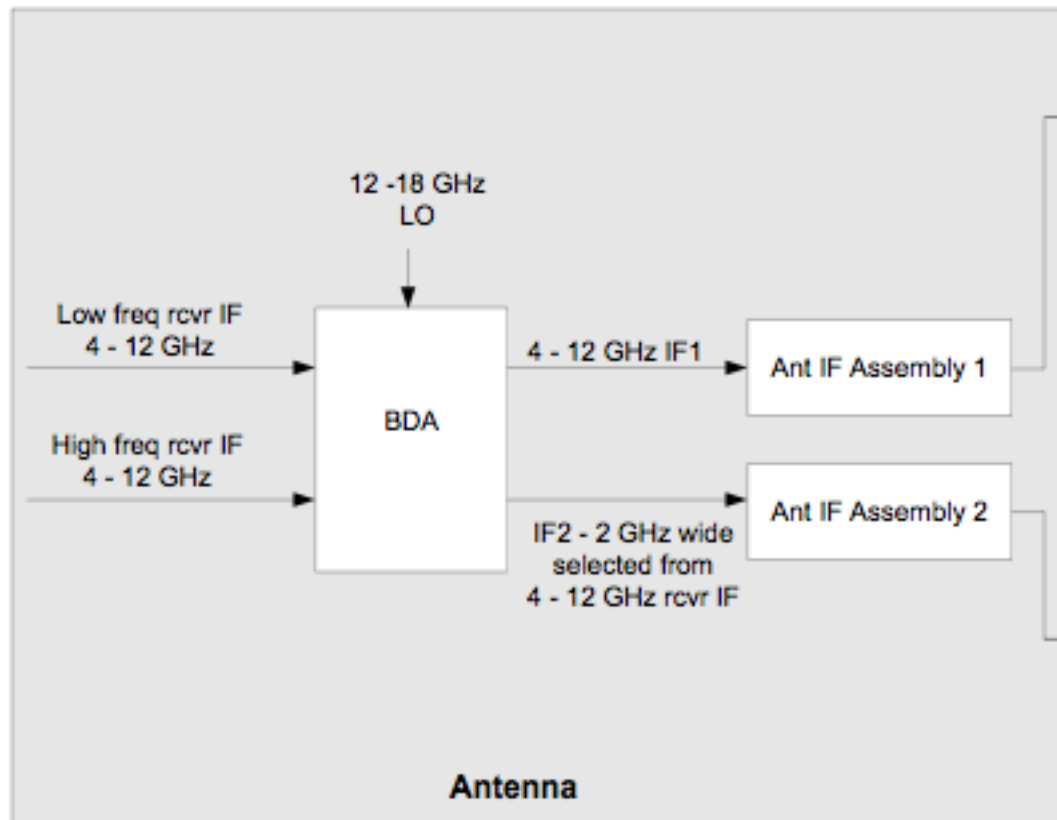


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Bandwidth Doubler Assembly (BDA)



BDA provides access to the expanded IF through an extra down-conversion in each antenna.

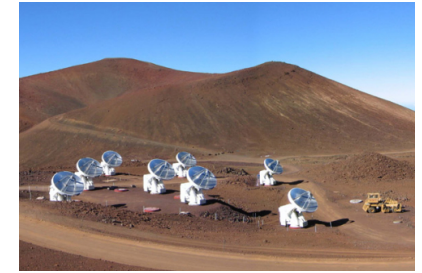
Increases throughput for single receiver operation.

Great tool for the commissioning of the SWARM correlator.



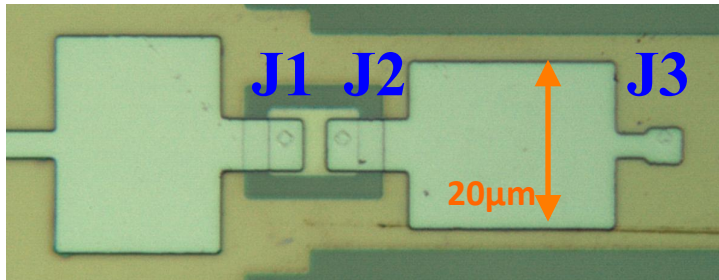
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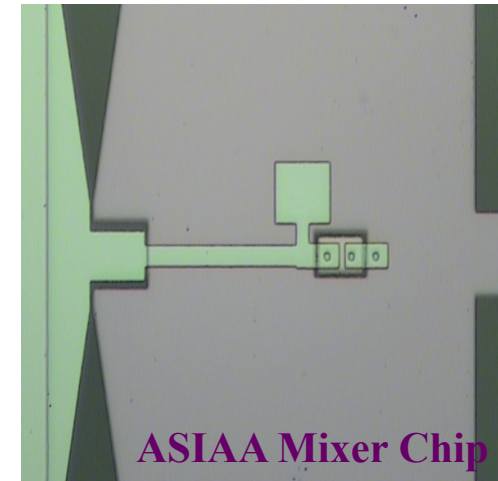


300 GHz Receiver Upgrade

- Initial Mixer Chips came from IRAM



- Junction size $\sim 1.1 \mu\text{m}^2$ (E-beam written)
- $J_c \sim 8 \text{ kA/cm}^2$ with low leakage
- Requires larger magnetic field
- Design is a scaled version of SMA-200
- Tuned to lower frequency because of larger spreading inductance.



ASIAA Mixer Chip

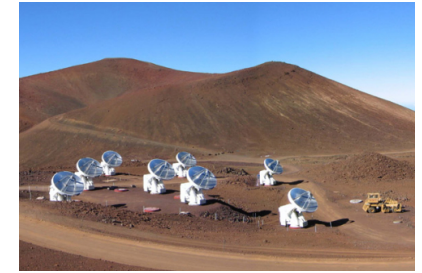
- Junction: $1.5 \mu\text{m}$ diameter
- $J_c \sim 7 \text{ kA/cm}^2$ with acceptable leakage ($R_{sg}/R_n \sim 10$)
- More compact design with low output capacitance ($C_{IF} \sim 0.18 \text{ pF}$)
- Design tuned to higher frequency.

As of end 2013, half of SMA-300 is upgraded with IRAM chips and half with ASIAA chips.

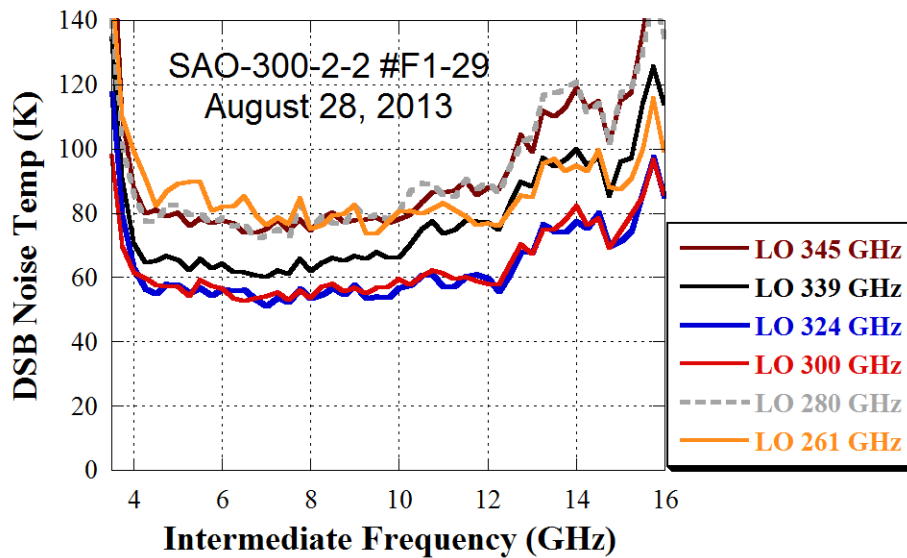


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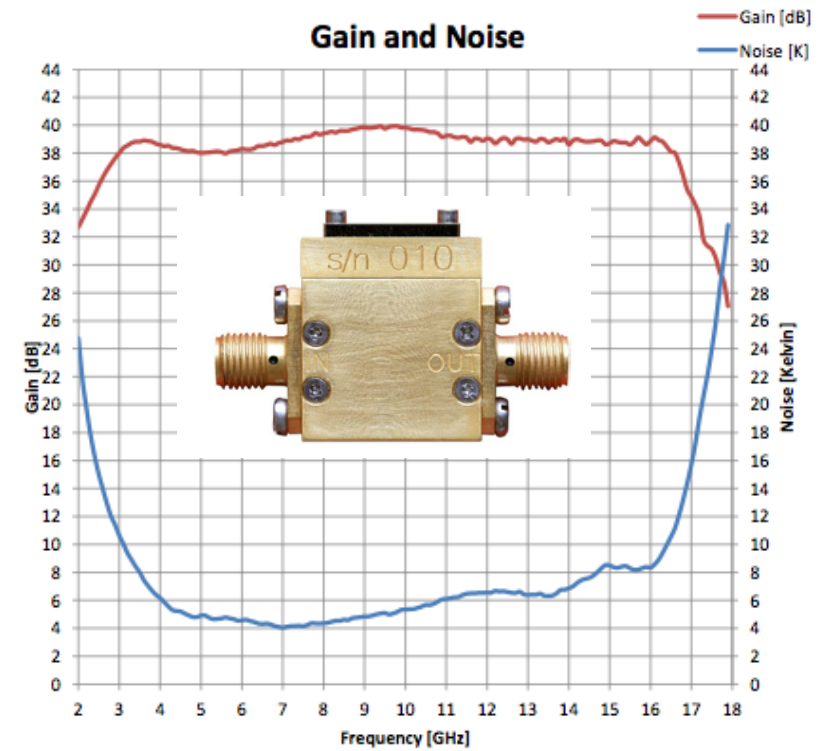


Wideband SMA-300 GHz Lab Data (in wet cryostat)



**IF > 12 GHz made possible with
new 4 – 16 GHz LNA from Sweden.**

Measured data, $T_{amb}=9$ K

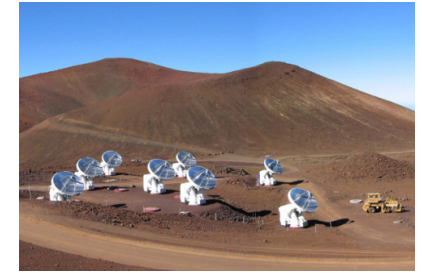


Low Noise Factory #LNF-LNC4_16A



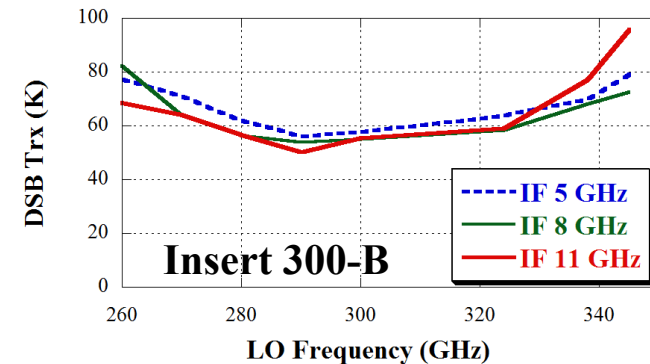
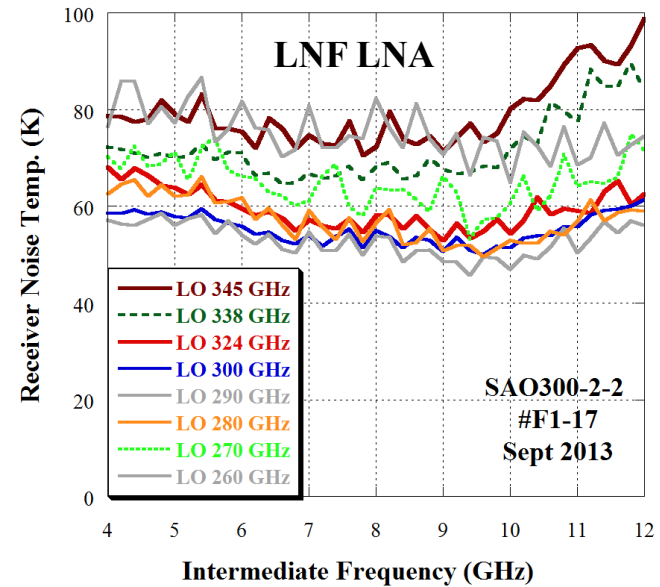
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Status of SMA-300 Receiver Set

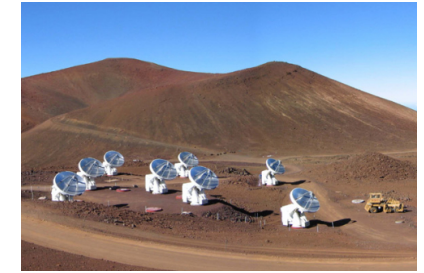
- **Upgraded to wideband chips end of 2013.**
- **Employs CRYO1-12 (Sandy) as LNA**
- **First unit with LNF amplifier to come online soon which should improve performance at high IF.**
- **Excellent sensitivity at mid-band (LO ~ 300 GHz)**
- **Sensitivity roll-off at 345 GHz due to lower conversion efficiency.**
- **Can be improved with lower leakage device.**





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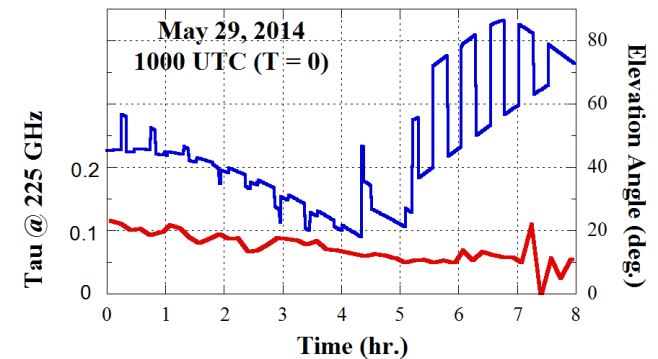
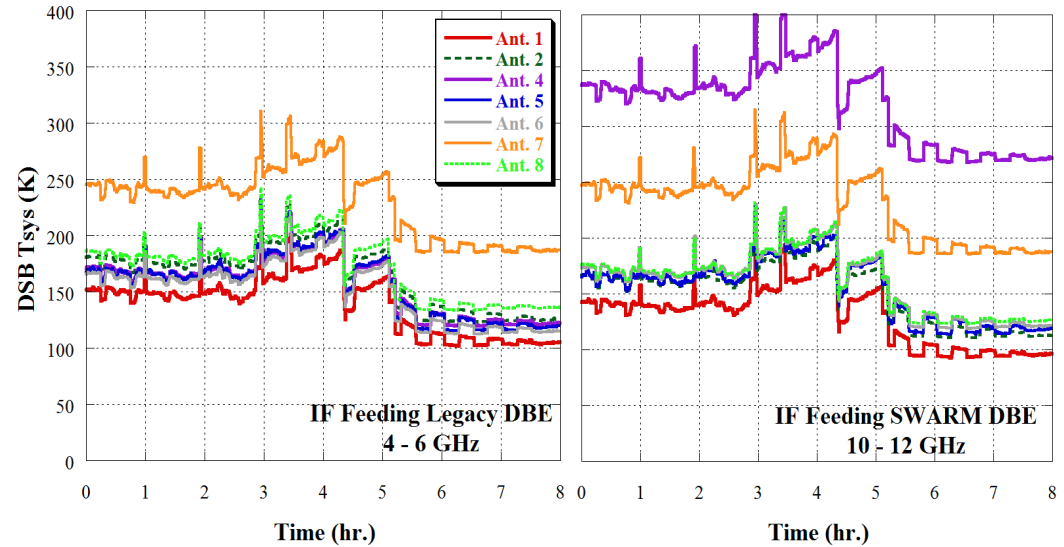
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On-Telescope Performance of 300 WB Receivers

- SWARM test on May 29
- LO 278.8 GHz
- Most antennas perform within a tight range of T_{sys} .

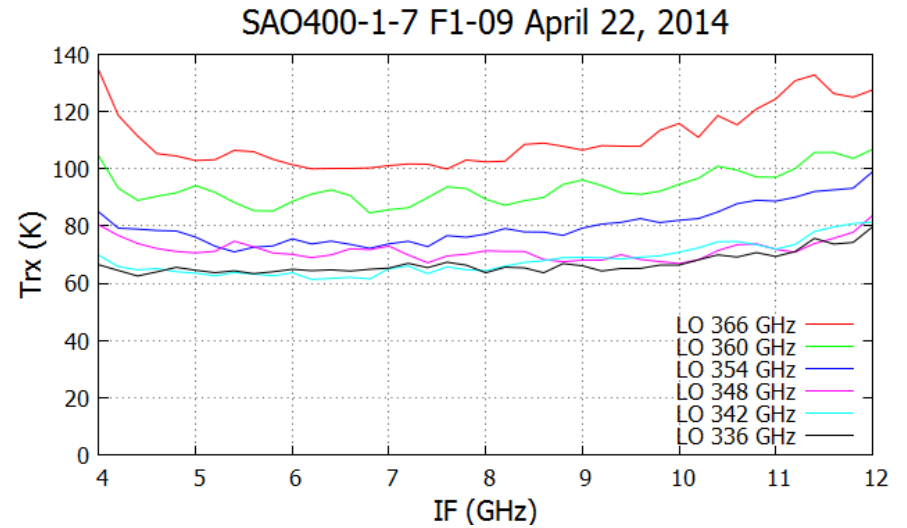
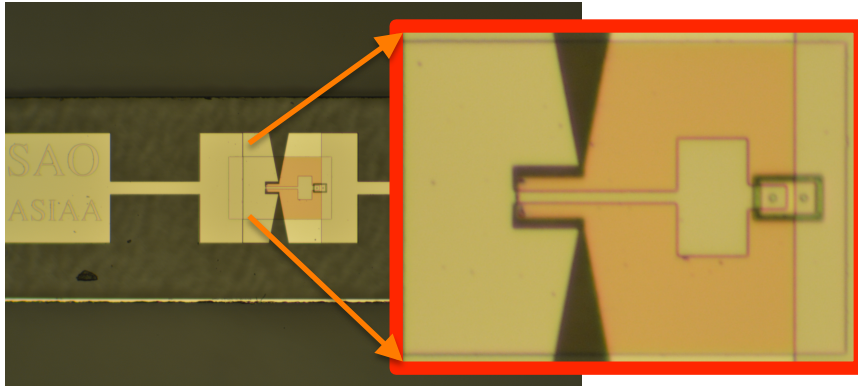
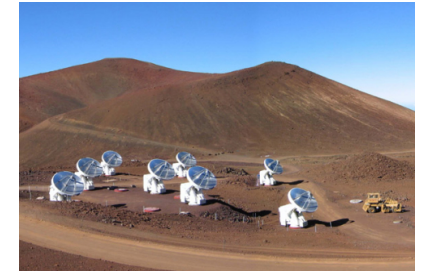
	T_{sys} (11G) / T_{sys} (5 G)
Ant. 1	0.94
Ant. 2	0.92
Ant. 4	2.00
Ant. 5	0.99
Ant. 6	1.05
Ant. 7	1.01
Ant. 8	0.94





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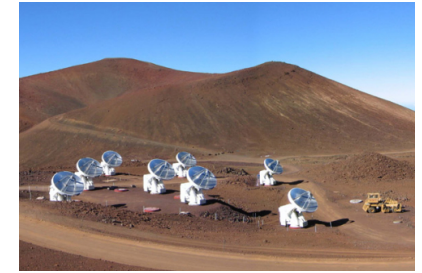
Ongoing 400 GHz Upgrade

- Design with 2-junction Array
- A few batches have been made by ASIAA
- Initial measurements performed in lab
- Junction size larger than design: mixer tuned low.
- Plan to install later this year pending on device supply.



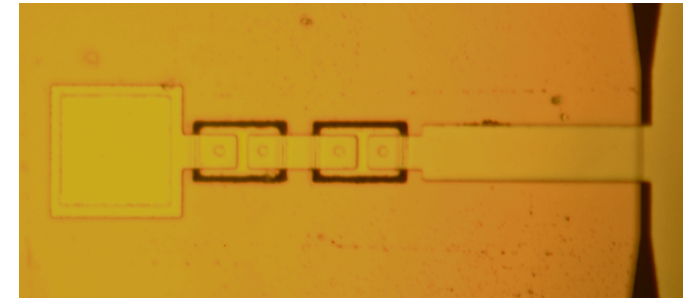
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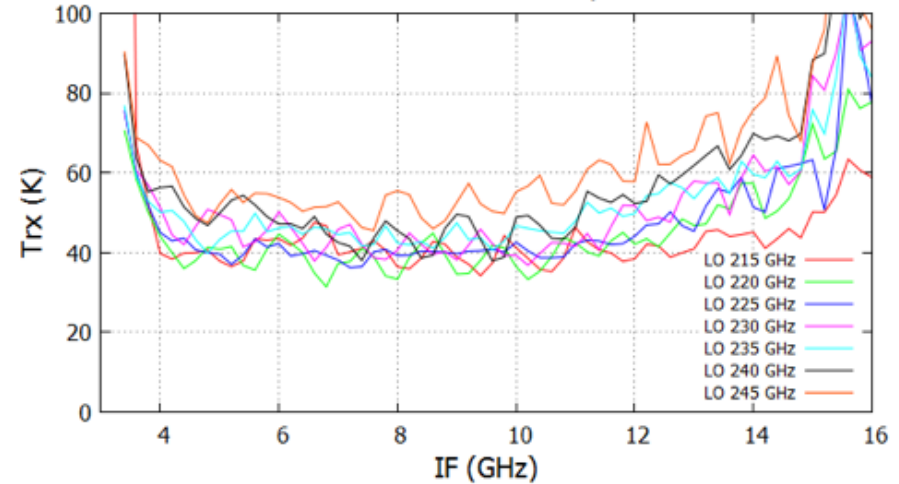


Ongoing 200 GHz Refinement

- The 3-junction design shows a drop in sensitivity above 11 GHz IF.
- Initial test with a 4-junction design in conjunction with the LNF amplifier gives good Trx up to 15 GHz IF.
- Refined 200 GHz mixers are expected to be in service by the end of 2014.



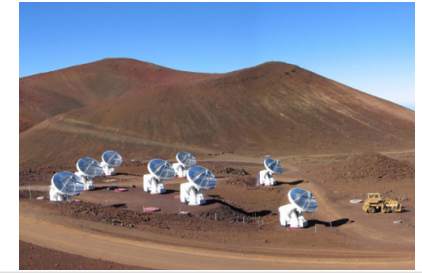
SAO200-4-8 #F2-01 May 28 2014



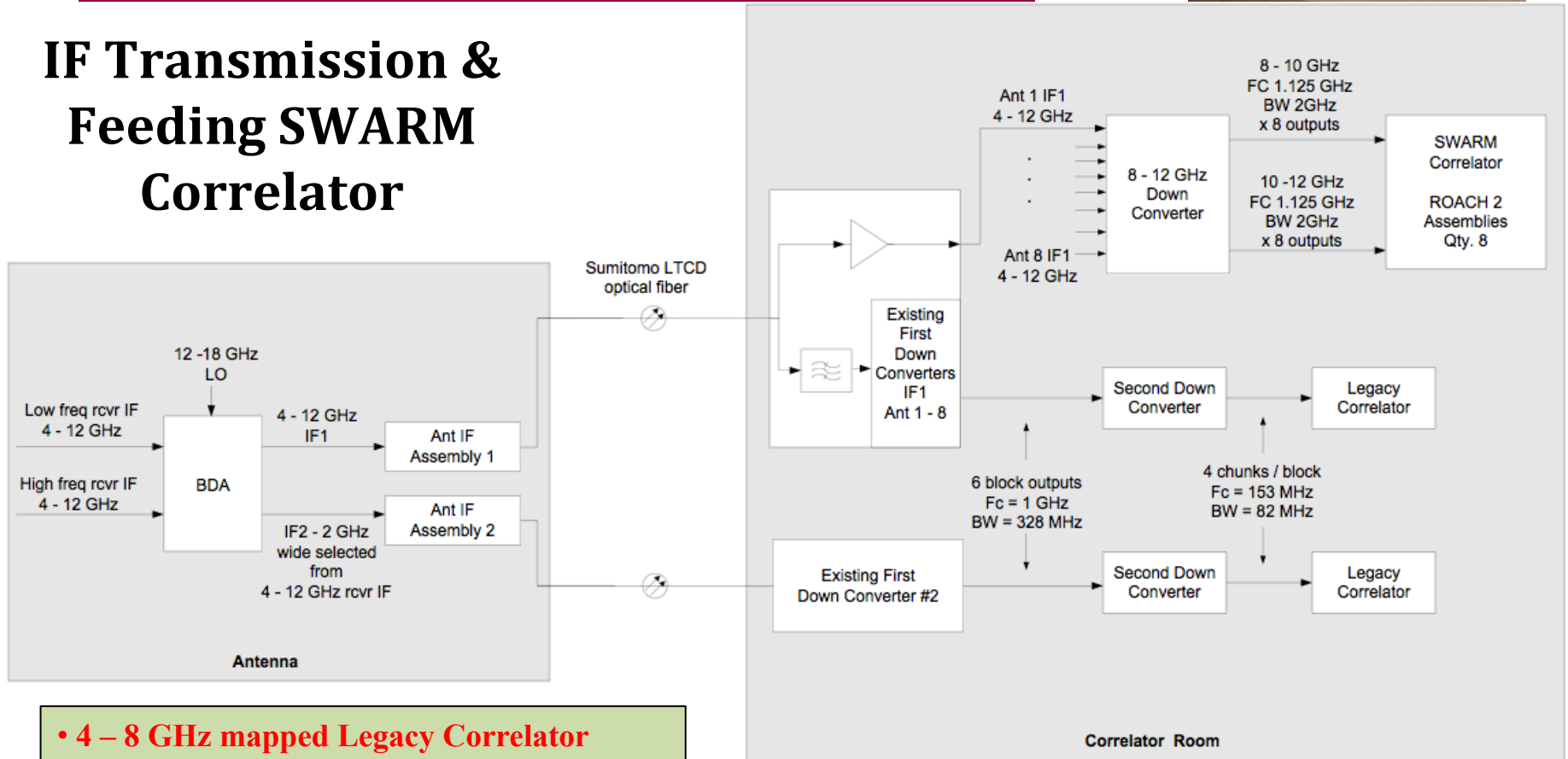


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IF Transmission & Feeding SWARM Correlator

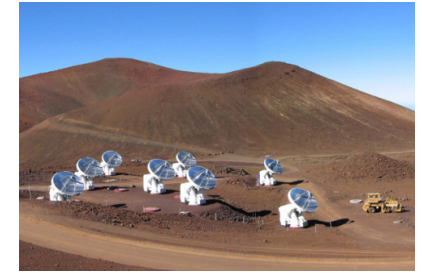


- 4 – 8 GHz mapped Legacy Correlator
- 8 – 12 GHz to SWARM Correlator
- Possibility of Dual 8 – 10 GHz on SWARM



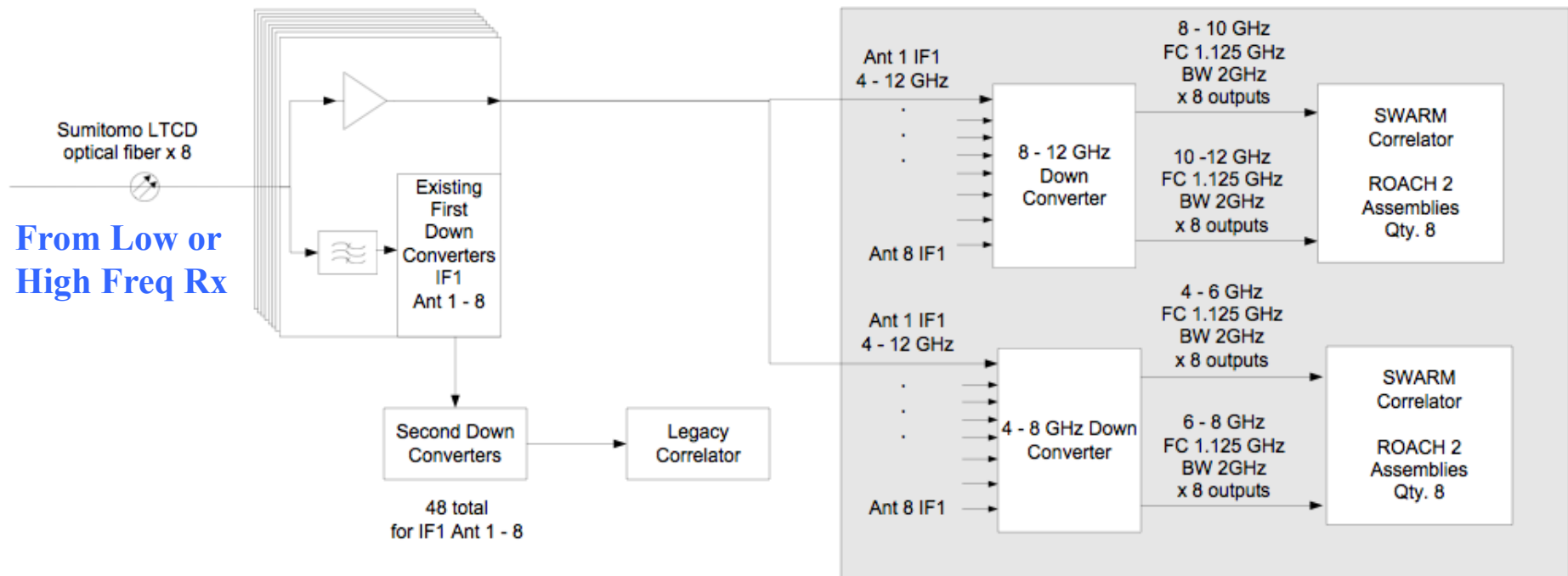
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Ongoing IF System Upgrade

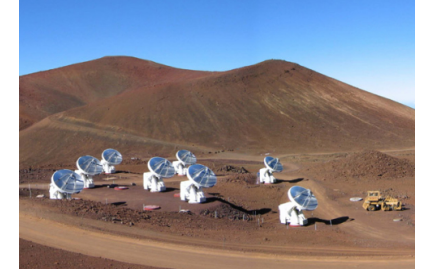
**New 4 – 8 GHz Downconverters will allow full SWARM operation on 4 – 12 GHz
And/or 2 x (4 – 8 GHz) dual receiver operation.**





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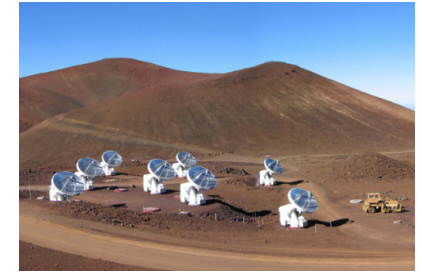
Medium Term Receiver Development Plans (2015 – 2016)

- **Currently SMA allows dual-pol observation at around 345 GHz. Propose to build one more receiver set (210 – 270 GHz) to allow dual-pol operation in the 200 GHz band.**
- **Upgrade all LNA with 4 – 16 GHz amplifiers to further expand IF band (requires more SWARM capacity).**
- **Build more IF processors to keep pace with SWARM expansion.**
- **Develop YIG-based LO unit to replace Gunn-based unit to streamline tuning.**



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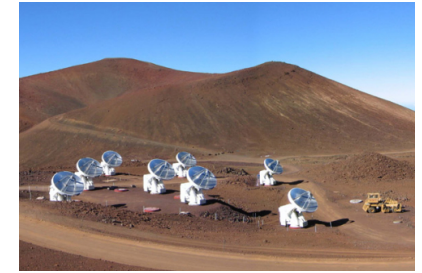
5-Year Time Scale Receiver Development Plan

- **460/490 GHz SSB Receiver Set**
- **2SB Receiver Set for 270 – 370 GHz**



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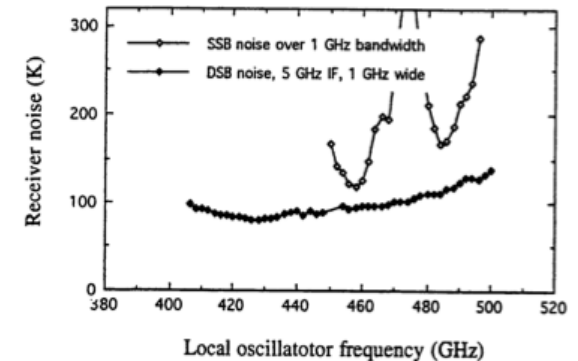
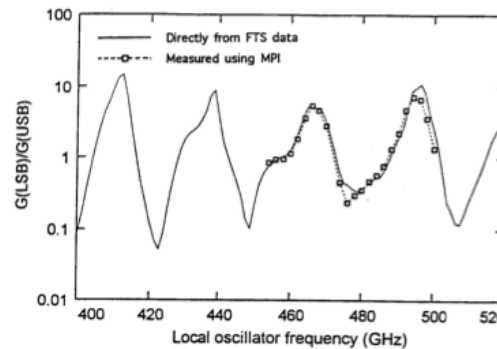
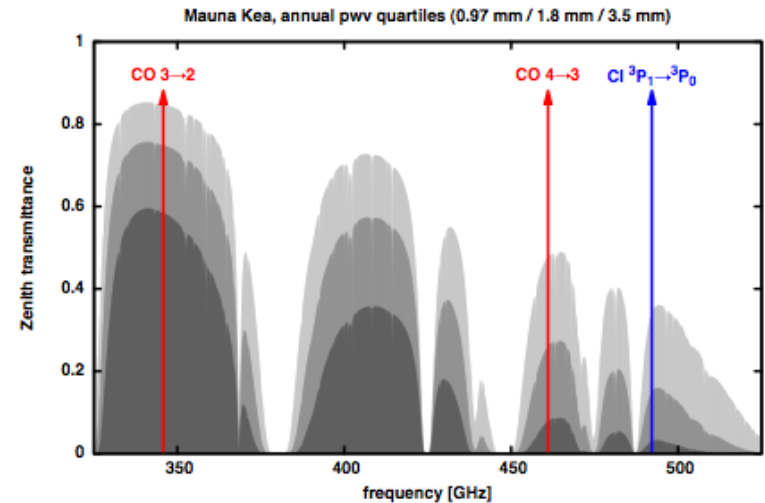
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460/490 GHz SSB Rx

In 1990s, we have experimented with a 460/490 SSB receiver using a fixed backshort which nulled the image frequency at ~ 475 GHz

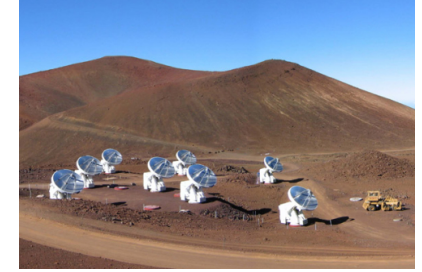
For projected $T_{SSB} \sim 100$ K, SSB Tsys to source of ~ 500 K (CO 4 – 3) and ~ 800 K (CI line) should readily be achievable.





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DSB Rx Vs 2SB Rx with Finite Image Rejection Ratio

Let the S/N ratio achieved by an SSB system be unity and α be the ratio of noise temperature.

$$\alpha = \frac{T_{\text{DSB}} \text{ (DSB system)}}{T_{\text{SSB}} \text{ (SSB system)}}$$

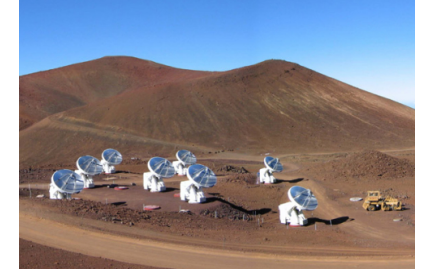
S/N ratio achieved by a DSB system compared to an SSB system	Infinite Image rejection ratio	Finite Image Rejection Ratio ρ
Continuum observation (both sidebands used)	$\frac{1}{\sqrt{2} \alpha}$	$\frac{1 + \rho}{\alpha \sqrt{2(1 + \rho^2)}}$
Spectral line observation (one side band used)	$\frac{1}{2 \alpha}$	$\frac{1 + \rho}{2 \alpha}$

REF: *Thompson & Kerr ALMA Memo #168*



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DSB Vs 2SB Receivers

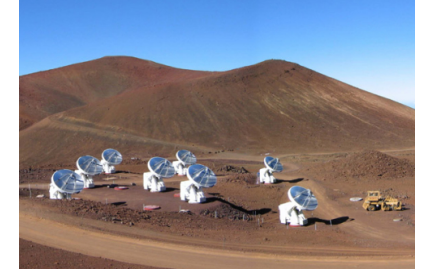
Result from AM model for Mauna Kea: assuming 1.4 mm PWV 45-deg source

		230 GHz $T_{\text{atm}}=32 \text{ K} \ \& \ T_{\text{R}}=35 \text{ K}$			345 GHz $T_{\text{atm}}=85 \text{ K} \ \& \ T_{\text{R}}=50 \text{ K}$		
$\alpha = \frac{T_{\text{DSB}}}{T_{\text{SSB}}} \approx \frac{T_{\text{atm}} + T_{\text{R}}}{T_{\text{atm}} + 2T_{\text{R}}}$		0.66			0.73		
Image Rejection Ratio ρ		∞	10 dB 0.1	6 dB 0.25	∞	10 dB 0.1	6 dB 0.25
DSB : USB Relative Sensitivity	Continuum	1.08	1.17	1.30	0.97	1.06	1.18
	Spectral Line	0.76	0.84	0.95	0.68	0.75	0.86



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- **With a given available correlator BW, there is no significant advantage for 2SB observation in continuum for both 230 and 345 GHz.**
- **Spectral line observation at 345 GHz, however, can be enhanced by a 2SB system.**
- **For frequencies above 345 GHz, the impact of atmosphere is more significant. 2SB system extending to 370 GHz would be useful.**
- **There is currently a development of waveguide LO injection receiver development for GLT at the Receiver Lab. So, it would be a parallel development.**
- **Price tag of such a receiver set would be of the order of \$1 million.**



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